

## Cantilever wall analysis

### Input data

#### Project

Task : OPORNI ZID ZA PARKIRIŠČE Z DOVOZNO CESTO POD POKOPALIŠČEM  
Customer : OBČINA ROGATEC  
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Project number : ZU 52/4/19

#### Settings

Slovenia - EN 1997

#### Materials and standards

Concrete structures : EN 1992-1-1 (EC2)  
Coefficients EN 1992-1-1 : standard

#### Wall analysis

Active earth pressure calculation : Coulomb  
Passive earth pressure calculation : Caquot-Kerisel  
Earthquake analysis : Mononobe-Okabe  
Shape of earth wedge : Calculate as skew  
Base key : The base key is considered as inclined footing bottom  
Allowable eccentricity : 0,333  
Verification methodology : according to EN 1997  
Design approach : 2 - reduction of actions and resistances

Partial factors on actions (A)				
Permanent design situation				
		Unfavourable		Favourable
Permanent actions :	$\gamma_G =$	1,35	[-]	1,00 [-]
Variable actions :	$\gamma_Q =$	1,50	[-]	0,00 [-]
Water load :	$\gamma_w =$	1,35	[-]	

Partial factors for resistances (R)				
Permanent design situation				
Partial factor on overturning :		$\gamma_{Rv} =$	1,40	[-]
Partial factor on sliding resistance :		$\gamma_{Rh} =$	1,10	[-]
Partial factor on bearing capacity :		$\gamma_{Re} =$	1,40	[-]

Partial factors for variable actions				
Permanent design situation				
Factor for combination value :		$\psi_0 =$	0,70	[-]
Factor for frequent value :		$\psi_1 =$	0,50	[-]
Factor for quasi-permanent value :		$\psi_2 =$	0,30	[-]

#### Material of structure

Unit weight  $\gamma = 25,00 \text{ kN/m}^3$

Analysis of concrete structures carried out according to the standard EN 1992-1-1 (EC2).

#### Concrete : C 25/30

Cylinder compressive strength  $f_{ck} = 25,00 \text{ MPa}$

Tensile strength  $f_{ctm} = 2,60 \text{ MPa}$

#### Longitudinal steel : B500

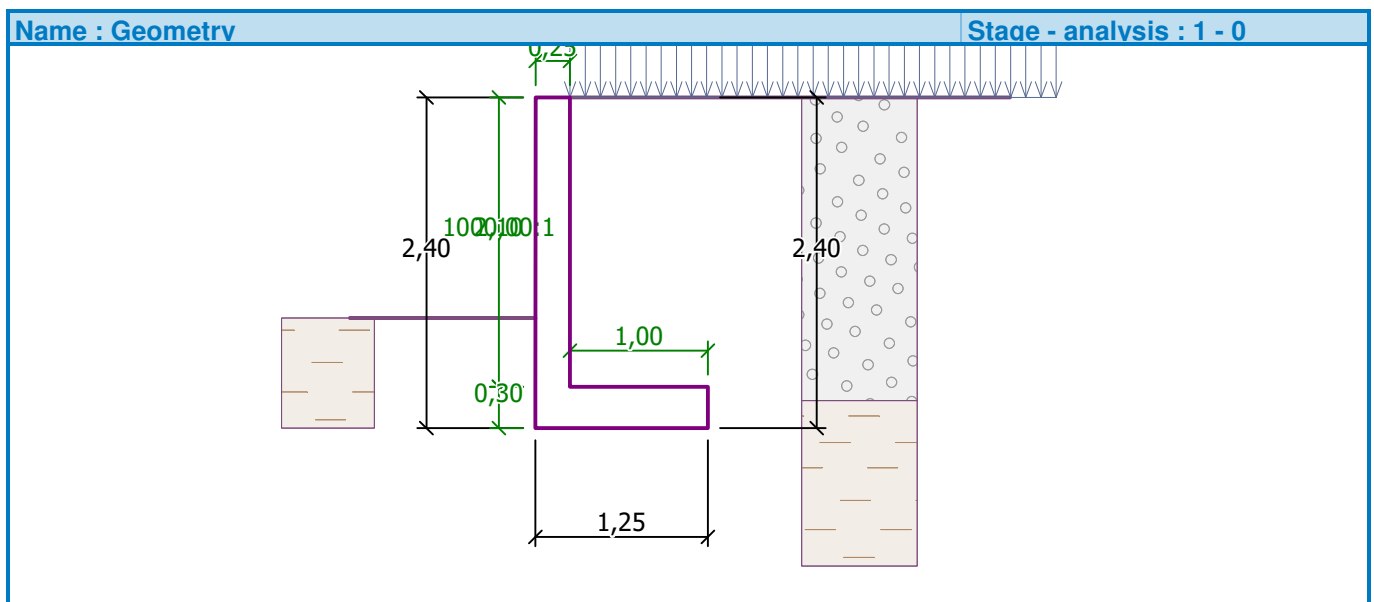
Yield strength

$$f_{yk} = 500,00 \text{ MPa}$$



### Geometry of structure

No.	Coordinate X [m]	Depth Z [m]
1	0,00	0,00
2	0,00	2,10
3	1,00	2,10
4	1,00	2,40
5	-0,25	2,40
6	-0,25	2,10
7	-0,25	0,00



The origin [0,0] is located at the most upper right point of the wall.  
Wall section area = 0,90 m<sup>2</sup>.



### Basic soil parameters

No.	Name	Pattern	$\Phi_{ef}$ [°]	$C_{ef}$ [kPa]	$\gamma$ [kN/m <sup>3</sup> ]	$\gamma_{su}$ [kN/m <sup>3</sup> ]	$\delta$ [°]
1	glina		18,00	2,00	16,00	8,00	0,00
2	tampon		35,00	0,00	20,00	12,00	0,00

### Soil parameters to compute pressure at rest

No.	Name	Pattern	Type calculation	$\Phi_{ef}$ [°]	$\nu$ [-]	OCR [-]	$K_r$ [-]
1	glina		cohesive	-	0,40	-	-
2	tampon		cohesionless	35,00	-	-	-

### Soil parameters



glina

Unit weight :  $\gamma = 16,00 \text{ kN/m}^3$   
 Stress-state : effective  
 Angle of internal friction :  $\varphi_{ef} = 18,00^\circ$   
 Cohesion of soil :  $c_{ef} = 2,00 \text{ kPa}$   
 Angle of friction struc.-soil :  $\delta = 0,00^\circ$   
 Soil : cohesive  
 Poisson's ratio :  $\nu = 0,40$   
 Saturated unit weight :  $\gamma_{sat} = 18,00 \text{ kN/m}^3$

#### tampon

Unit weight :  $\gamma = 20,00 \text{ kN/m}^3$   
 Stress-state : effective  
 Angle of internal friction :  $\varphi_{ef} = 35,00^\circ$   
 Cohesion of soil :  $c_{ef} = 0,00 \text{ kPa}$   
 Angle of friction struc.-soil :  $\delta = 0,00^\circ$   
 Soil : cohesionless  
 Saturated unit weight :  $\gamma_{sat} = 22,00 \text{ kN/m}^3$

#### Geological profile and assigned soils

No.	Layer [m]	Assigned soil	Pattern
1	2,20	tampon	
2	-	glina	

#### Foundation

Type of foundation : soil from geological profile

#### Terrain profile

Terrain behind the structure is flat.

#### Water influence

Ground water table is located below the structure.

#### Input surface surcharges

No.	Surcharge		Action	Mag.1 [kN/m <sup>2</sup> ]	Mag.2 [kN/m <sup>2</sup> ]	Ord.x x [m]	Length l [m]	Depth z [m]
	new	change						
1	Yes		variable	9,00				on terrain

#### Resistance on front face of the structure

Resistance on front face of the structure: passive

Soil on front face of the structure - glina

Angle of friction struc.-soil  $\delta = 0,00^\circ$

Soil thickness in front of structure  $h = 0,80 \text{ m}$

Terrain in front of structure is flat.

#### Settings of the stage of construction

Design situation : permanent

The wall is free to move. Active earth pressure is therefore assumed.

### Verification No. 1 (Stage of construction 1)

#### Forces acting on construction

Name	F <sub>hor</sub> [kN/m]	App.Pt. z [m]	F <sub>vert</sub> [kN/m]	App.Pt. x [m]	Coeff. overtur.	Coeff. sliding	Coeff. stress
Weight - wall	0,00	-0,85	22,57	0,33	1,000	1,000	1,350
FF resistance	-14,28	-0,31	0,01	0,00	1,000	1,000	1,350
Weight - earth wedge	0,00	-0,94	19,21	0,59	1,000	1,000	1,350
Active pressure	17,35	-0,73	22,79	0,89	1,350	1,350	1,350
Surch.1 - surface	6,32	-1,12	9,00	0,75	1,500	1,500	1,500

#### Verification of complete wall

##### Check for overturning stability

Resisting moment  $M_{res} = 40,29$  kNm/m

Overturning moment  $M_{ovr} = 23,30$  kNm/m

**Wall for overturning is SATISFACTORY**

##### Check for slip

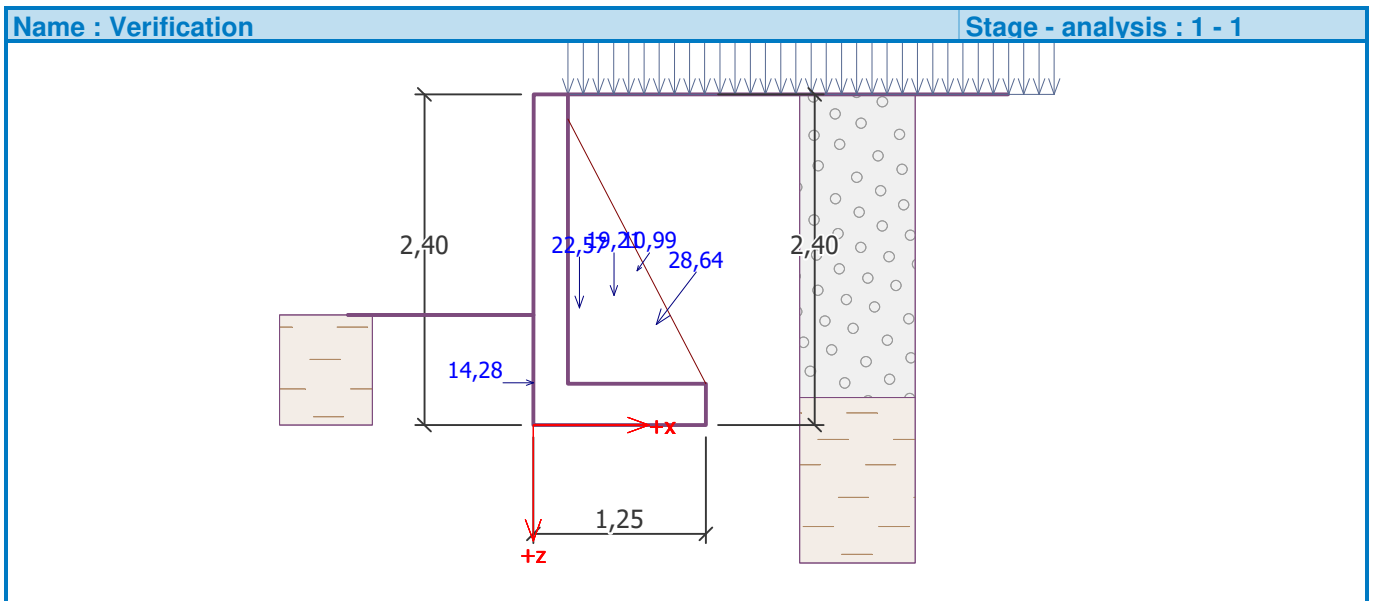
Resisting horizontal force  $H_{res} = 26,82$  kN/m

Active horizontal force  $H_{act} = 18,62$  kN/m

**Wall for slip is SATISFACTORY**

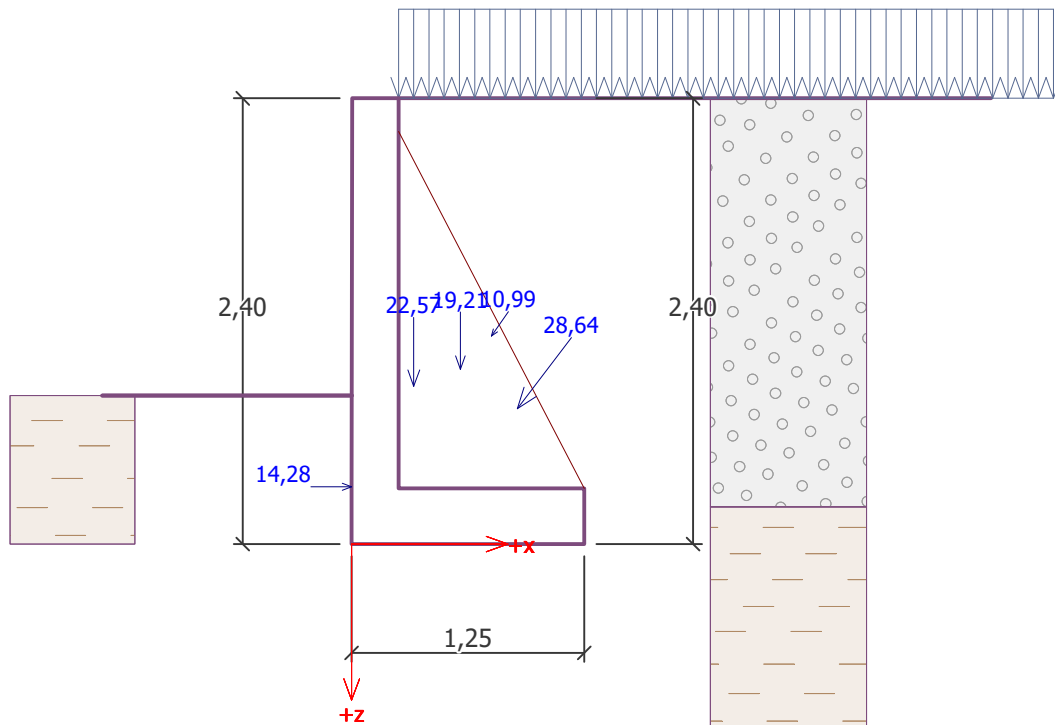
**Overall check - WALL is SATISFACTORY**

Maximum stress in footing bottom : 122,93 kPa



Name : Verification

Stage - analysis : 1 - 1



### Bearing capacity of foundation soil (Stage of construction 1)

Design load acting at the center of footing bottom

No.	Moment [kNm/m]	Norm. force [kN/m]	Shear Force [kN/m]	Eccentricity [-]	Stress [kPa]
1	21,80	100,68	13,62	0,173	122,93
2	20,76	86,05	18,62	0,193	111,82

Service load acting at the center of footing bottom

No.	Moment [kNm/m]	Norm. force [kN/m]	Shear Force [kN/m]
1	15,49	73,58	9,39

### Dimensioning No. 1 (Stage of construction 1)

Forces acting on construction

Name	F <sub>hor</sub> [kN/m]	App.Pt. z [m]	F <sub>vert</sub> [kN/m]	App.Pt. x [m]	Coeff. moment	Coeff. norm.force	Coeff. shear for.
Weight - wall	0,00	-1,05	13,17	0,13	1,000	1,350	1,000
FF resistance	-6,59	-0,20	0,01	0,00	1,000	1,350	1,000
Pressure at rest	18,78	-0,70	0,00	0,25	1,350	1,000	1,350
Surch.1 - surface	8,05	-1,05	0,00	0,25	1,500	0,000	1,500

### Wall stem check

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 50,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,25 m

Reinforcement ratio  $\rho = 0,20 \% > 0,14 \% = \rho_{min}$

Position of neutral axis  $x = 0,01 m < 0,12 m = x_{max}$

Ultimate shear force  $V_{Rd} = 97,56 \text{ kN} > 30,85 \text{ kN} = V_{Ed}$   
 Ultimate moment  $M_{Rd} = 32,78 \text{ kNm} > 29,09 \text{ kNm} = M_{Ed}$

**Cross-section is SATISFACTORY.**

## Dimensioning No. 2 (Stage of construction 1)

### Forces acting on construction

Name	$F_{hor}$ [kN/m]	App.Pt. z [m]	$F_{vert}$ [kN/m]	App.Pt. x [m]	Coeff. moment	Coeff. norm.force	Coeff. shear for.
Weight - wall	0,00	-1,05	13,17	0,13	1,000	1,350	1,000
FF resistance	-6,59	-0,20	0,01	0,00	1,000	1,350	1,000
Pressure at rest	18,78	-0,70	0,00	0,25	1,350	1,000	1,350
Surch.1 - surface	8,05	-1,05	0,00	0,25	1,500	0,000	1,500

### Wall check at the construction joint 2,10 m from the wall crest

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 50,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,25 m

Reinforcement ratio  $\rho = 0,20 \% > 0,14 \% = \rho_{min}$

Position of neutral axis  $x = 0,01 \text{ m} < 0,12 \text{ m} = x_{max}$

Ultimate shear force  $V_{Rd} = 97,56 \text{ kN} > 30,85 \text{ kN} = V_{Ed}$

Ultimate moment  $M_{Rd} = 32,78 \text{ kNm} > 29,09 \text{ kNm} = M_{Ed}$

**Cross-section is SATISFACTORY.**

## Dimensioning No. 3 (Stage of construction 1)

### Forces acting on construction

Name	$F_{hor}$ [kN/m]	App.Pt. z [m]	$F_{vert}$ [kN/m]	App.Pt. x [m]	Design coefficient
Weight - wall	0,00	-0,15	7,50	0,75	1,350
Weight - earth wedge	0,00	-0,94	19,21	0,59	1,350
Active pressure	17,35	-0,73	22,79	0,89	1,350
Surch.1 - surface	6,32	-1,12	9,00	0,75	1,500
Contact stress	0,00	0,00	-63,60	0,58	1,000

### Back wall jump check

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 30,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,30 m

Reinforcement ratio  $\rho = 0,15 \% > 0,14 \% = \rho_{min}$

Position of neutral axis  $x = 0,01 \text{ m} < 0,16 \text{ m} = x_{max}$



Ultimate shear force  $V_{Rd} = 118,47 \text{ kN} > 16,73 \text{ kN} = V_{Ed}$

Ultimate moment  $M_{Rd} = 44,37 \text{ kNm} > 19,46 \text{ kNm} = M_{Ed}$

**Cross-section is SATISFACTORY.**

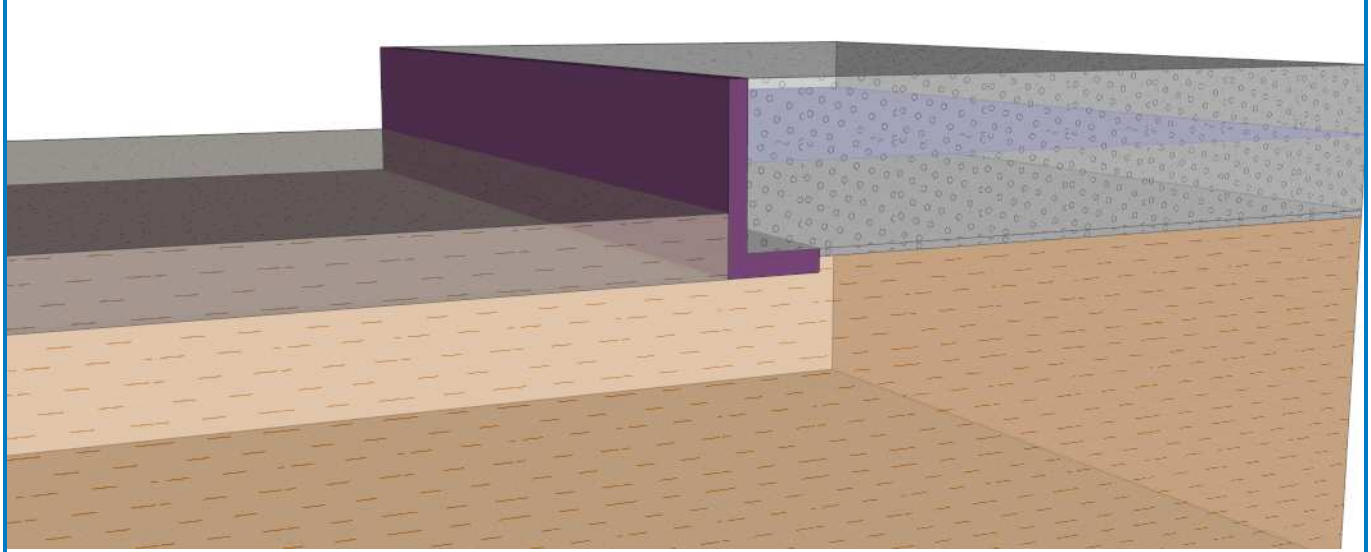
## Input data (Stage of construction 2)

### Geological profile and assigned soils

No.	Layer [m]	Assigned soil	Pattern
1	2,20	tampon	
2	-	glina	

Name : Profile and assignment

Stage - analysis : 2 - 0



#### Foundation

Type of foundation : soil from geological profile

#### Terrain profile

Terrain behind the structure is flat.

#### Water influence

GWT behind the structure lies at a depth of 1,00 m  
Uplift in foot. bottom due to different pressures is not considered.

#### Resistance on front face of the structure

Resistance on front face of the structure: passive

Soil on front face of the structure - glina

Angle of friction struc.-soil  $\delta = 0,00^\circ$

Soil thickness in front of structure  $h = 0,80$  m

Terrain in front of structure is flat.

#### Settings of the stage of construction

Design situation : permanent

The wall is free to move. Active earth pressure is therefore assumed.

### Verification No. 1 (Stage of construction 2)

#### Forces acting on construction

Name	F <sub>hor</sub> [kN/m]	App.Pt. z [m]	F <sub>vert</sub> [kN/m]	App.Pt. x [m]	Coeff. overtur.	Coeff. sliding	Coeff. stress
Weight - wall	0,00	-0,85	22,57	0,33	1,000	1,000	1,350
FF resistance	-14,28	-0,31	0,01	0,00	1,000	1,000	1,350
Weight - earth wedge	0,00	-1,02	12,93	0,56	1,000	1,000	1,350
Active pressure	14,69	-0,79	20,27	0,87	1,350	1,350	1,350
Water pressure	9,80	-0,47	0,00	0,25	1,350	1,350	1,000
Uplift pressure	0,00	-2,40	0,00	0,25	1,000	1,000	1,000

#### Verification of complete wall

##### Check for overturning stability

Resisting moment  $M_{res} = 27,64$  kNm/m

Overturning moment  $M_{ovr} = 17,46$  kNm/m

**Wall for overturning is SATISFACTORY**

##### Check for slip

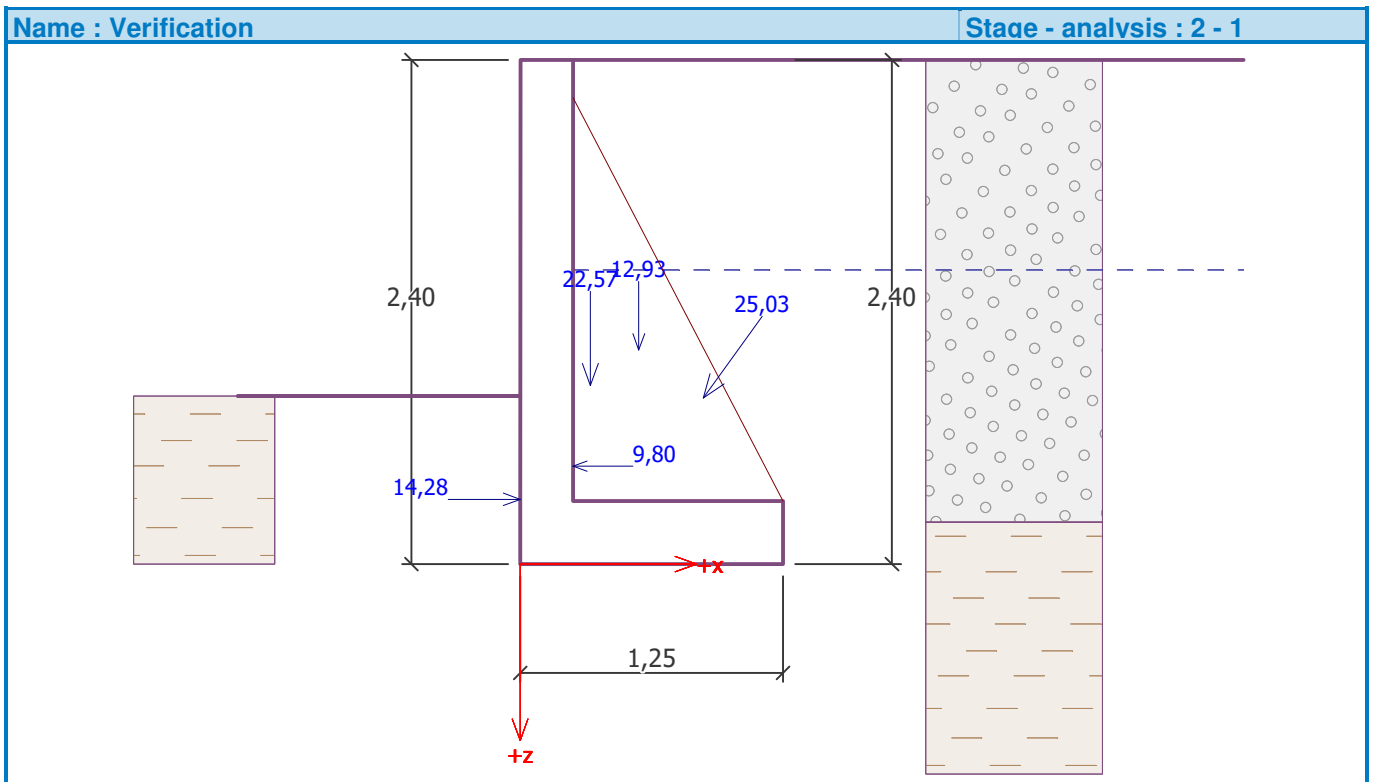
Resisting horizontal force  $H_{res} = 19,80$  kN/m

Active horizontal force  $H_{act} = 18,78$  kN/m

**Wall for slip is SATISFACTORY**

**Overall check - WALL is SATISFACTORY**

Maximum stress in footing bottom : 95,84 kPa



### Bearing capacity of foundation soil (Stage of construction 2)

#### Design load acting at the center of footing bottom



No.	Moment [kNm/m]	Norm. force [kN/m]	Shear Force [kN/m]	Eccentricity [-]	Stress [kPa]
1	17,56	75,30	10,36	0,186	95,84
2	18,12	62,87	18,78	0,230	93,03

#### Service load acting at the center of footing bottom

No.	Moment [kNm/m]	Norm. force [kN/m]	Shear Force [kN/m]
1	14,19	55,78	10,21

#### Verification of foundation soil

Stress in the footing bottom : rectangle

#### Eccentricity verification

Max. eccentricity of normal force  $e = 0,230$

Maximum allowable eccentricity  $e_{alw} = 0,333$

**Eccentricity of the normal force is SATISFACTORY**

#### Verification of bearing capacity

Bearing capacity of foundation soil  $R = 200,00$  kPa

Partial factor on bearing capacity  $\gamma_{Rv} = 1,40$

Max. stress at footing bottom  $\sigma = 95,84$  kPa

Bearing capacity of foundation soil  $R_d = 142,86$  kPa

**Bearing capacity of foundation soil is SATISFACTORY**

**Overall verification - bearing capacity of found. soil is SATISFACTORY**

### Dimensioning No. 1 (Stage of construction 2)

#### Forces acting on construction

Name	$F_{hor}$ [kN/m]	App.Pt. z [m]	$F_{vert}$ [kN/m]	App.Pt. x [m]	Coeff. moment	Coeff. norm.force	Coeff. shear for.
Weight - wall	0,00	-1,05	13,17	0,13	1,000	1,350	1,000
FF resistance	-6,59	-0,20	0,01	0,00	1,000	1,350	1,000
Pressure at rest	16,72	-0,74	0,00	0,25	1,350	1,000	1,350
Water pressure	6,04	-0,37	0,00	0,25	1,350	1,000	1,350
Uplift pressure	0,00	-2,10	0,00	0,25	1,000	1,000	1,000

#### Wall stem check

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 50,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,25 m

Reinforcement ratio  $\rho = 0,20$  % > 0,14 % =  $\rho_{min}$

Position of neutral axis  $x = 0,01$  m < 0,12 m =  $x_{max}$

Ultimate shear force  $V_{Rd} = 97,56$  kN > 24,14 kN =  $V_{Ed}$

Ultimate moment  $M_{Rd} = 32,78$  kNm > 18,38 kNm =  $M_{Ed}$

**Cross-section is SATISFACTORY.**

## Dimensioning No. 2 (Stage of construction 2)

### Forces acting on construction

Name	F <sub>hor</sub> [kN/m]	App.Pt. z [m]	F <sub>vert</sub> [kN/m]	App.Pt. x [m]	Coeff. moment	Coeff. norm.force	Coeff. shear for.
Weight - wall	0,00	-1,05	13,17	0,13	1,000	1,350	1,000
FF resistance	-6,59	-0,20	0,01	0,00	1,000	1,350	1,000
Pressure at rest	16,72	-0,74	0,00	0,25	1,350	1,000	1,350
Water pressure	6,04	-0,37	0,00	0,25	1,350	1,000	1,350
Uplift pressure	0,00	-2,10	0,00	0,25	1,000	1,000	1,000

### Wall check at the construction joint 2,10 m from the wall crest

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 50,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,25 m

Reinforcement ratio  $\rho = 0,20 \% > 0,14 \% = \rho_{min}$

Position of neutral axis  $x = 0,01 \text{ m} < 0,12 \text{ m} = x_{max}$

Ultimate shear force  $V_{Rd} = 97,56 \text{ kN} > 24,14 \text{ kN} = V_{Ed}$

Ultimate moment  $M_{Rd} = 32,78 \text{ kNm} > 18,38 \text{ kNm} = M_{Ed}$

**Cross-section is SATISFACTORY.**

## Dimensioning No. 3 (Stage of construction 2)

### Forces acting on construction

Name	F <sub>hor</sub> [kN/m]	App.Pt. z [m]	F <sub>vert</sub> [kN/m]	App.Pt. x [m]	Design coefficient
Weight - wall	0,00	-0,15	7,50	0,75	1,350
Weight - earth wedge	0,00	-1,02	12,93	0,56	1,350
Active pressure	14,69	-0,79	20,27	0,87	1,350
Contact stress	0,00	0,00	-46,53	0,56	1,000

### Back wall jump check

Reinforcement and dimensions of the cross-section

5 prof. 10,0 mm, cover 50,0 mm

Cross-section width = 1,00 m

Cross-section depth = 0,30 m

Reinforcement ratio  $\rho = 0,16 \% > 0,14 \% = \rho_{min}$

Position of neutral axis  $x = 0,01 \text{ m} < 0,15 \text{ m} = x_{max}$

Ultimate shear force  $V_{Rd} = 112,60 \text{ kN} > 8,41 \text{ kN} = V_{Ed}$

Ultimate moment  $M_{Rd} = 40,96 \text{ kNm} > 13,10 \text{ kNm} = M_{Ed}$

**Cross-section is SATISFACTORY.**

## Slope stability analysis

### Input data

#### Project

#### Settings

Slovenia - EN 1997

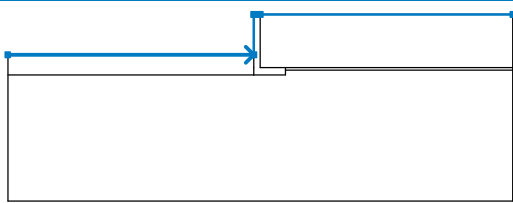
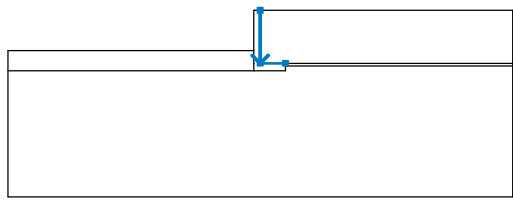
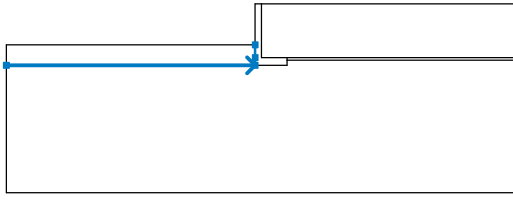
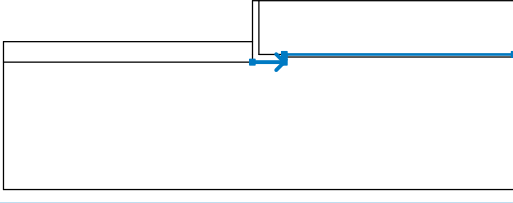
### Stability analysis

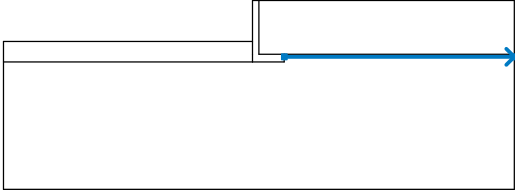
Earthquake analysis : Standard  
 Verification methodology : according to EN 1997  
 Design approach : 3 - reduction of actions (GEO, STR) and soil parameters

Partial factors on actions (A)					
Permanent design situation					
		State STR		State GEO	
		Unfavourable	Favourable	Unfavourable	Favourable
Permanent actions :	$\gamma_G =$	1,00 [-]	1,00 [-]	1,00 [-]	1,00 [-]
Variable actions :	$\gamma_Q =$	1,50 [-]	0,00 [-]	1,30 [-]	0,00 [-]
Water load :	$\gamma_w =$			1,00 [-]	


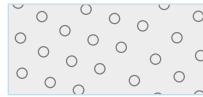
Partial factors for soil parameters (M)		
Permanent design situation		
Partial factor on internal friction :	$\gamma_\phi =$	1,25 [-]
Partial factor on effective cohesion :	$\gamma_c =$	1,25 [-]
Partial factor on undrained shear strength :	$\gamma_{cu} =$	1,40 [-]

### Interface



No.	Interface location	Coordinates of interface points [m]					
		x	z	x	z	x	z
1		-10,00	0,60	-0,25	0,60	-0,25	2,20
		0,00	2,20	10,00	2,20		
2		0,00	2,20	0,00	0,10	1,00	0,10
3		-10,00	-0,20	-0,25	-0,20	-0,25	0,10
		-0,25	0,60				
4		-0,25	-0,20	1,00	-0,20	1,00	0,00
		1,00	0,10	10,00	0,10		

No.	Interface location	Coordinates of interface points [m]					
		x	z	x	z	x	z
5		1,00	0,00	10,00	0,00		

### Soil parameters - effective stress state

No.	Name	Pattern	$\phi_{ef}$ [°]	$c_{ef}$ [kPa]	$\gamma$ [kN/m <sup>3</sup> ]
1	glina		18,00	2,00	16,00
2	tampon		35,00	0,00	20,00

### Soil parameters - uplift

No.	Name	Pattern	$\gamma_{sat}$ [kN/m <sup>3</sup> ]	$\gamma_s$ [kN/m <sup>3</sup> ]	n [-]
1	glina		18,00		
2	tampon		22,00		

### Soil parameters

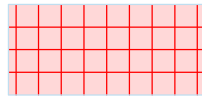
#### glina

Unit weight :  $\gamma = 16,00 \text{ kN/m}^3$   
 Stress-state : effective  
 Angle of internal friction :  $\phi_{ef} = 18,00^\circ$   
 Cohesion of soil :  $c_{ef} = 2,00 \text{ kPa}$   
 Saturated unit weight :  $\gamma_{sat} = 18,00 \text{ kN/m}^3$

#### tampon

Unit weight :  $\gamma = 20,00 \text{ kN/m}^3$   
 Stress-state : effective  
 Angle of internal friction :  $\phi_{ef} = 35,00^\circ$   
 Cohesion of soil :  $c_{ef} = 0,00 \text{ kPa}$   
 Saturated unit weight :  $\gamma_{sat} = 22,00 \text{ kN/m}^3$

### Rigid bodies

No.	Name	Sample	$\gamma$ [kN/m <sup>3</sup> ]
1	Wall material		25,00

### Assigning and surfaces

No.	Surface position	Coordinates of surface points [m]				Assigned soil
		x	z	x	z	
1		10,00	0,10	10,00	2,20	tampon 
		0,00	2,20	0,00	0,10	
		1,00	0,10			
2		10,00	0,00	10,00	0,10	tampon 
		1,00	0,10	1,00	0,00	
3		1,00	-0,20	1,00	0,00	Wall material 
		1,00	0,10	0,00	0,10	
		0,00	2,20	-0,25	2,20	
		-0,25	0,60	-0,25	0,10	
4		-0,25	-0,20	-0,25	0,10	glina 
		-0,25	0,60	-10,00	0,60	
		-10,00	-0,20			
5		1,00	0,00	1,00	-0,20	glina 
		-0,25	-0,20	-10,00	-0,20	
		-10,00	-5,20	10,00	-5,20	
		10,00	0,00			

### Water

Water type : GWT

No.	GWT location	Coordinates of GWT points [m]					
		x	z	x	z	x	z
1		-10,00	-0,20	0,00	-0,20	0,00	1,20
		10,00	1,20				

### Tensile crack

Tensile crack not input.

### Earthquake

Earthquake not included.

### Settings of the stage of construction

Design situation : permanent

## Results (Stage of construction 1)

### Analysis 1

#### Circular slip surface

Slip surface parameters					
Center :	x =	-0,44 [m]	Angles :	$\alpha_1 =$	-55,19 [°]
	z =	2,21 [m]		$\alpha_2 =$	89,80 [°]
Radius :	R =	2,82 [m]			
The slip surface after optimization.					

#### Slope stability verification (Bishop)

Sum of active forces :  $F_a = 46,30$  kN/m

Sum of passive forces :  $F_p = 50,25$  kN/m

Sliding moment :  $M_a = 130,57$  kNm/m

Resisting moment :  $M_p = 141,72$  kNm/m

Utilization : 92,1 %

**Slope stability ACCEPTABLE**

